



CHE392-Chemical Engineering Laboratory I

Online Education Term

5B- UNSTEADY STATE HEAT TRANSFER

THEORY

Heat transfer may occur by any one or more of the three basic mechanisms of heat transfer:

Conduction: The heat is conducted by the transfer of the energy of motion between adjacent molecules. In conduction, energy can also be transferred by free electrons.

The transfer of heat by conduction follows this basic equation and is written as Fourier's Law for heat conduction in fluids or solids:

$$Q = -k \cdot A \cdot (dT/dx)$$

Q: Heat transfer rate in W

A: Cross-sectional area normal to the direction of flow of heat in m^2

T: Temperature in K

x: Distance in m

k: Thermal conductivity in W/m.K

2. Convection: The transfer of heat by convection implies the transfer of heat by bulk transport and mixing of macroscopic elements of warmer portions with cooler portions of a gas or liquid.

Q: Heat transfer rate in W

A: Area in m^2

T_f: Average of bulk temperature of fluid flowing past in K

T_w: Temperature of the solid surface in K

h: Convective heat transfer coefficient W/ m^2 .K

$$Q = h \cdot A \cdot (T_f - T_w)$$

3. Radiation: Radiation is the transfer of energy through space by means of electromagnetic waves in much the same way as electromagnetic light waves transfer light.

The net heat of absorption is then, by the Stefan-Boltzmann equation:

$$Q = \sigma \cdot A \cdot T^4$$

Q: Heat flow in W

A: Surface area of body in m^2

σ : Constant 5.676×10^{-8} W/ m^2 .K⁴

T: Temperature of the black body in K

Dimensionless Number

- **Nusselt Number:** Nu is used to relate data for the heat transfer coefficient h to the thermal conductivity k of the fluid and a characteristic dimension D .

$$Nu = \frac{hD}{k}$$

- **Prandtl Number:** Pr is the ratio of the shear component of diffusivity for momentum μ/ρ to the diffusivity for heat $k/\rho \cdot c_p$.

$$Pr = \frac{c_p \mu}{k}$$

- **Reynold Number:** Ratio of kinetic or inertial forces to the viscous forces in the fluid stream.

$$Re = \frac{D \cdot V \cdot \rho}{\mu}$$

- **Biot Number:** Biot number compares the relative values of internal conduction resistance and surface convective resistance to heat transfer.

$$Bi = \frac{h l}{k}$$

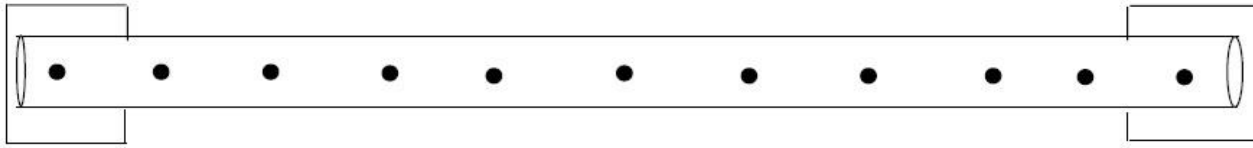
- **Grashof Number:** Ratio of forcing (buoyancy) forces to restraining (viscous) forces.

$$Gr = \frac{g \beta (T_w - T_\infty) D^3}{k}$$

Objective

- The purpose is to examine the temperature distribution along the brass rod maintained at two fixed temperatures and the heat loss from this rod.
- In this experiment, we will study processes in which the temperature at any given point in the system changes with time, that is, heat transfer is unsteady state or transient.

Experimental Setup



- It is a cylindrical rod that is heated by electric power from its end sides and placed in a thermometer in various positions along its length.
- 11 thermometers are placed on the approximately 1 meter long brass rod.





- The two ends of the cylindrical brass rod are heated to 150°C with electrical resistances and are kept constant at this temperature.
- Every 10 minutes, the temperatures are read from the thermometers placed along the rod at the same time.
- This process lasts up to 10 minutes after the thermometers in the rod have reached 150°C .
- The obtained data are recorded in the table.
- The ambient temperature is also measured.

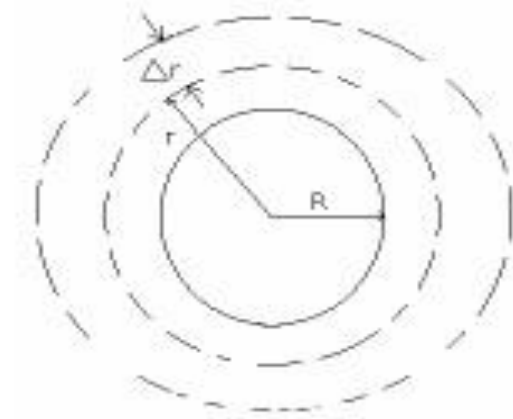
HEAT TRANSFER THROUGH STAGNANT FLUID ENVIRONMENT FROM CYLINDER SURFACE

Assumptions:

Cylinder outer surface temperature $T_w = \text{constant}$

Steady state

In the case of $\partial r = 785R$ $T = T_\infty$



$$\frac{(2\pi r L)q|_r - (2\pi r L)q|_{r+\Delta r}}{(2\pi r)\Delta r} = 0$$

$$\lim_{\Delta r \rightarrow 0} \left(\frac{r q|_r - r q|_{r+\Delta r}}{\Delta r} \right) = 0 \Rightarrow -\frac{d(qr)}{dr} = 0 \quad -q = \frac{c_1}{r} \quad q = -hA \frac{dT}{dr} \quad \longrightarrow \quad -\left(-hA \frac{dT}{dr} \right) = \frac{c_1}{r} \quad \frac{dT}{dr} = \frac{c_1}{hAr} \quad T = c' \ln r + c_2$$

Boundary condition

$$T = T_w \quad r = R$$

$$T_w = c' \ln R + c_2$$

$$T = T_\infty \quad r = 785R$$

$$T_\infty = c' \ln 785R + c_2$$

$$T_w - T_\infty = c'(\ln R - \ln 785R)$$

$$T_w - T_\infty = c' \ln \frac{R}{785R} \Rightarrow c' = \frac{T_w - T_\infty}{\ln \left(\frac{R}{785R} \right)}$$

$$c' = \frac{(T_w - T_\infty)}{-6,666}$$

$$q|_{r=R} = ?$$

$$q|_{r=R} = (2\pi RL)\left(-k\frac{dT}{dr}\right)|_{r=R} = -2\pi RLk\frac{C_1}{r}\bigg|_{r=R} = -2\pi RLk\frac{(T_w - T_\infty)}{(-6,666)R} = \frac{\pi Lk}{3,333}(T_w - T_\infty)$$

$$q|_{r=R} = \frac{\pi Lk}{3,333}(T_w - T_\infty) \equiv h(T_w - T_\infty)(2\pi RL) \Rightarrow \frac{k}{3,333} = hD \Rightarrow \frac{hD}{k} = 0,3 \quad \Rightarrow \quad \text{Nu}=0,3$$

HEAT TRANSFER BY NATURAL CONVECTION FROM HORIZONTAL CYLINDER

- Average temperature of the cylindrical bar T_w
- Ambient temperature T_∞

Film temperature (T_f)

300K	350K
$\rho = 1.1774 \text{ kg/m}^3$	$\rho = 0.9980 \text{ kg/m}^3$
$C_p = 1.0057 \text{ kJ/kg.K}$	$C_p = 1.0090 \text{ kJ/kg.K}$
$\mu = 1.8462 \times 10^{-5} \text{ kg/m.s}$	$\mu = 2.075 \times 10^{-5} \text{ kg/m.s}$
$\nu = 15.69 \times 10^{-6} \text{ m}^2/\text{s}$	$\nu = 20.76 \times 10^{-6} \text{ m}^2/\text{s}$
$k = 0.02624 \text{ W/m.K}$	$k = 0.03003 \text{ W/m.K}$
$Pr = 0.708$	$Pr = 0.697$

Nusselt Number

$$Nu = \frac{hD}{k}$$

$$Nu = c Ra^n$$

$$Gr \rightarrow Ra \rightarrow Nu \rightarrow h \rightarrow q$$

Prandtl Number

$$Pr = \frac{C_p \mu}{k}$$

Grashof Number

$$Gr = \frac{g\beta(T_w - T_\infty)D^3}{\gamma^2}$$

Rayling Number

$$Ra = Gr \cdot Pr$$

Ra	c	n
10^{-10} - 10^{-2}	0.675	0.058
10^{-2} - 10^2	1.02	0.148
10^2 - 10^4	0.85	0.188
10^4 - 10^7	0.48	0.25
10^7 - 10^{12}	0.125	0.333

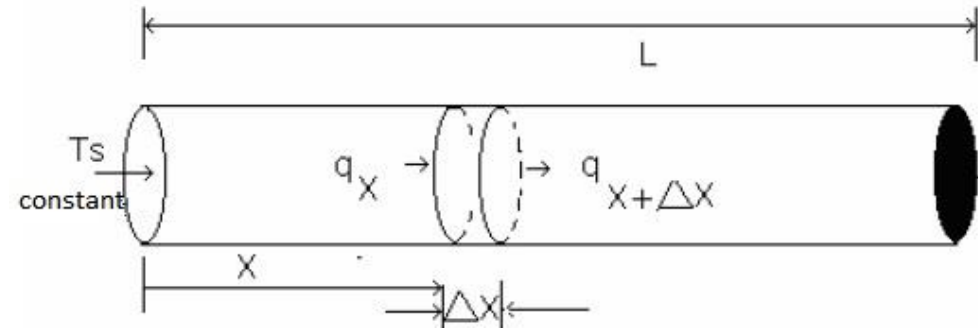
HEAT LOSS FROM CYLINDRICAL FIN (STEADY STATE)

$$\theta = (T - T_{\infty}); \quad m^2 = \frac{hP}{kA} \quad \Rightarrow \quad \frac{\partial^2 \theta}{\partial x^2} = m^2 \theta$$

$$\theta = C_1 e^{-mx} + C_2 e^{+mx} \quad C_1 = \theta_s \frac{e^{mL}}{(e^{mL} + e^{-mL})} \quad ; \quad C_2 = \theta_s \frac{e^{-mL}}{(e^{mL} + e^{-mL})}$$

$$\frac{\theta}{\theta_s} = \frac{e^{m(L-x)} + e^{-m(L-x)}}{e^{mL} + e^{-mL}} \quad \frac{\theta}{\theta_s} = \frac{\cosh m(L-x)}{\cosh mL}$$

$$Bi = \frac{h\ell'}{k} \quad \ell' = \frac{PL^2}{A} \quad Q = k.A.m.(T_w - T_{\infty}).\tanh mL$$



UNSTEADY STATE HEAT TRANSFER FROM HORIZONTAL ROD WHOSE ENDS ARE KEPT AT CONSTANT TEMPERATURE

$$A.q|_x - A.q|_{x+\Delta x} - h.(T - T_\infty).P.\Delta x = \rho.C_p.A.\Delta x.\frac{dT}{dt}$$

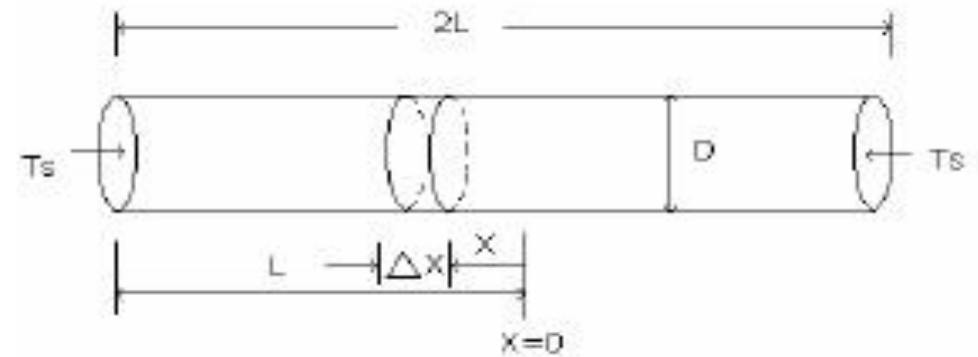
$$A\left(-k\frac{dT}{dx}\right)|_x - A\left(-k\frac{dT}{dx}\right)|_{x+\Delta x} - h.(T - T_\infty).P.\Delta x = \rho.C_p.A.\Delta x.\frac{dT}{dt}$$

$$\frac{\partial^2 T}{\partial x^2} - \frac{h.P}{k.A}(T - T_\infty) = \frac{\rho.C_p.A}{k.A} \times \frac{\partial T}{\partial t} \quad \frac{\partial Q}{\partial t} = \frac{\partial T}{\partial t} \Rightarrow \frac{d^2 Q}{dt^2} = \frac{d^2 T}{dt^2}$$

$$t=0 \quad T=T_\infty \quad U=(T_i - T_\infty)$$

$$x=L \quad T=T_s \quad U=(T_s - T_\infty)e^{\beta t} = Q_s e^{\beta t}$$

$$x=-L \quad T=T_s \quad U=(T_s - T_\infty)e^{-\beta t}$$



$$Q = Q_s \times \frac{\cosh x \left(\frac{\beta}{\alpha} \right)^{1/2}}{\cosh L \left(\frac{\beta}{\alpha} \right)^{1/2}} - \frac{4Q_s}{\pi} \times \sum_{n=0}^{\infty} \frac{(-1)^n e^{-\beta t} - \left[\frac{\alpha(2n+1)^2 \pi^2 t}{4L^2} \right] \times \cos \left[\frac{(2n+1)\pi x}{2L} \right]}{(2n+1) \left[1 + \frac{4\beta.L^2}{(2n+1)^2 \pi^2 \alpha} \right]}$$

$$Q = Q_s \frac{\cosh x \left(\frac{\beta}{\alpha} \right)^{1/2}}{\cosh L \left(\frac{\beta}{\alpha} \right)^{1/2}} - 0$$

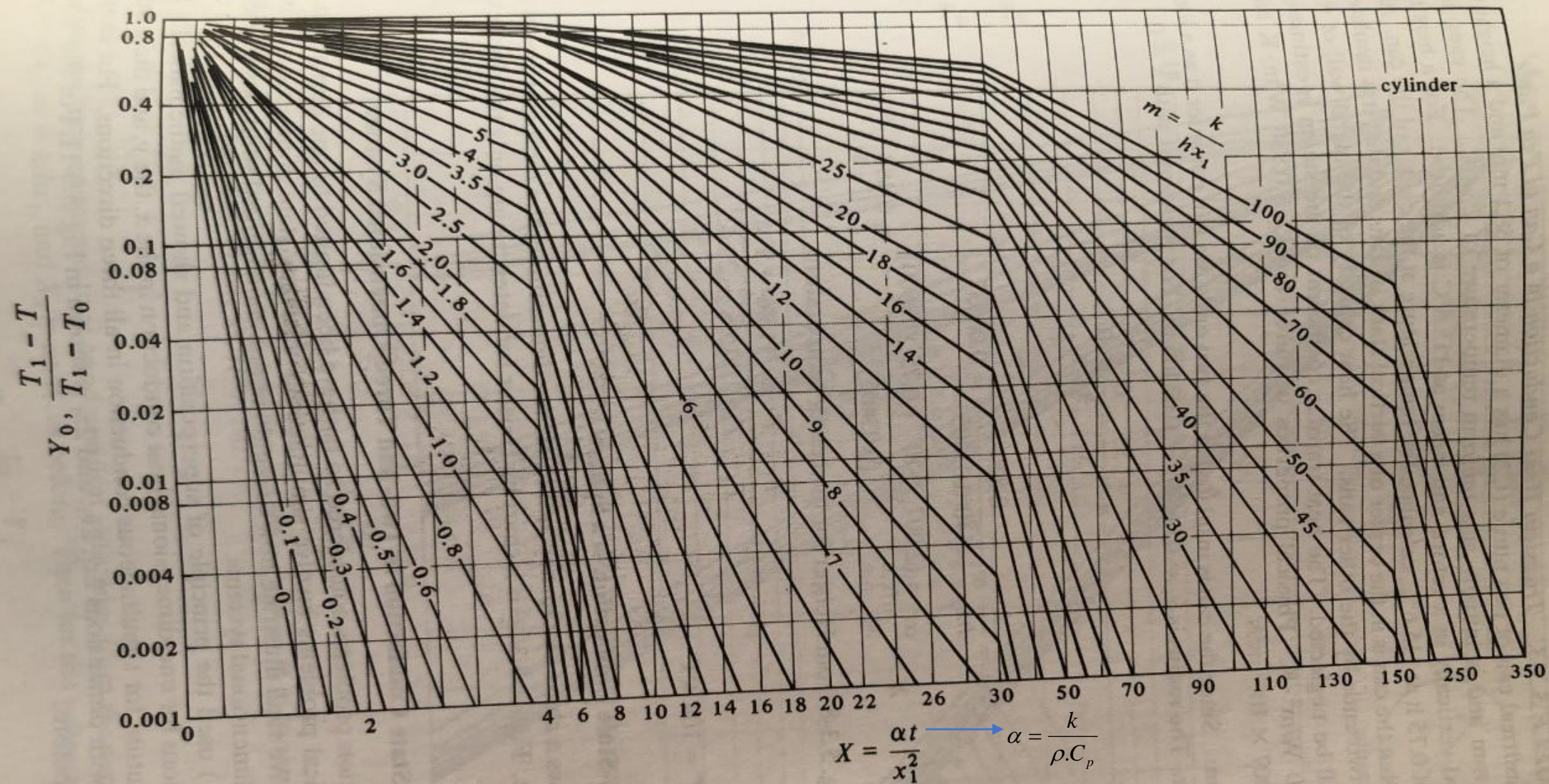
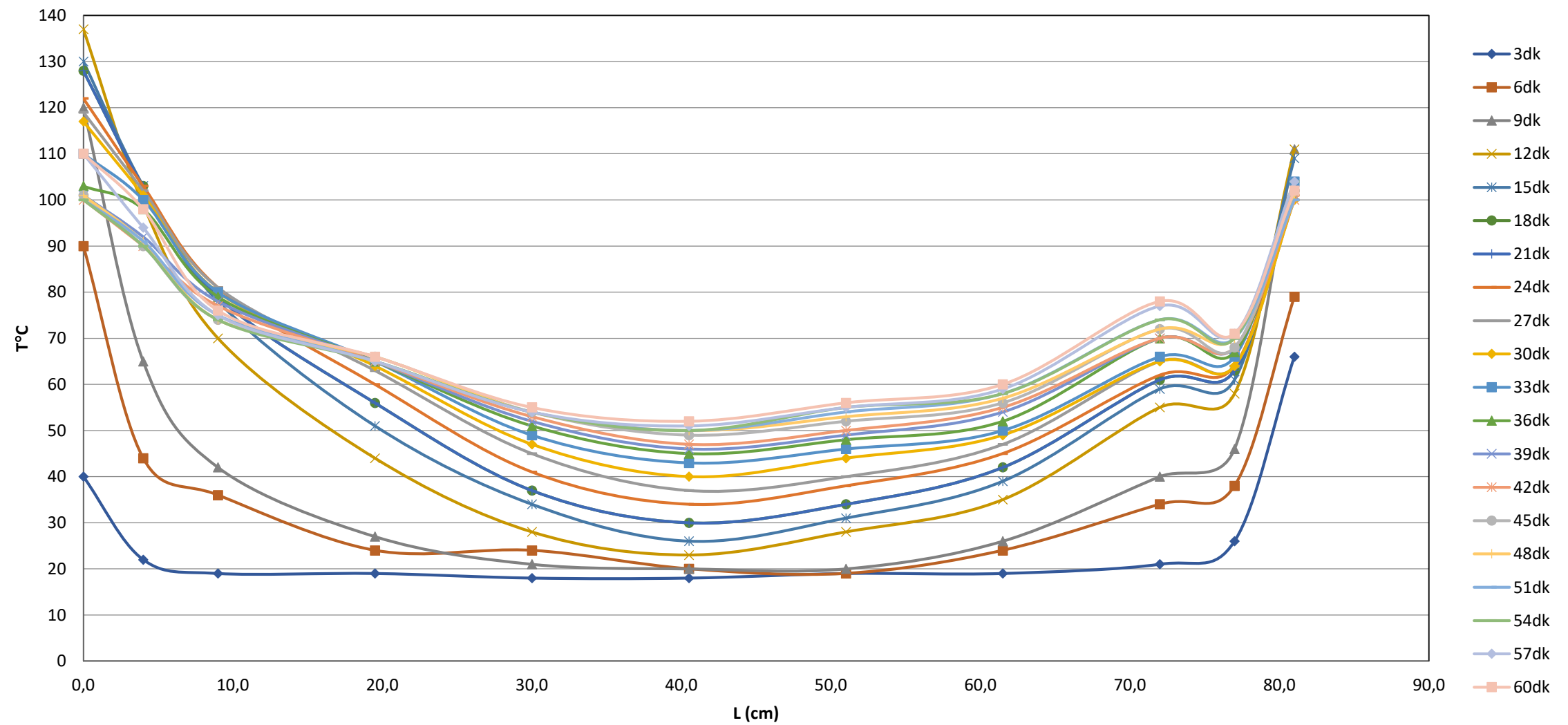


FIGURE 5.3-8. Chart for determining temperature at the center of a long cylinder for unsteady-state heat conduction. [From H. P. Heisler, Trans. A.S.M.E., 69, 227 (1947). With permission.]



Data Table

Row Number	T ₁	T ₂	T ₃	T ₄	T ₅	T ₆	T ₇	T ₈	T ₉	T ₁₀	T ₁₁
1											
2											
3											
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